INFLUENCE OF THE TYPE OF ADHESIVE ON THE PHYSICO-MECHANICAL PROPERTIES OF BEND FURNITURE BOARDS

Vladimir Mihailov, Todor Petkov University of Forestry, Sofia, Bulgaria e-mail: vladko86mihailov@gmail.com; todor ltu@mail.bg

ABSTRACT

In the manufacture of furniture structural elements from folded glued thin furniture panels, it is important to determine the parameters affecting the performance of the finished wood composite panels. The purpose of the study was to determine the effect of the type of adhesive used on laminated high-density laminated wood fiber boards (HDF) and poplar plywood. The test specimens are made of five layers of 2.8 mm thick HDF slats and 4 mm thick plywood with 260/100 mm glued plate dimensions. For bonding, three types of adhesives were used - polyvinyl acetate (PVA) dispersion adhesive Jowacoll 103.05, polyurethane (PU) dispersion adhesive - Jovapur 150.50 and polyurethane wood adhesive - SOUDAL 66A. Bending and gluing were performed in a laboratory vacuum press with a rubber membrane and a template with a radius of curvature of 150 mm. The time to achieve minimum technological adhesion strength, vacuum velocity and minimum bending radius are determined. Samples were tested by standard bending with shoulder collection. The results obtained are analyzed and presented graphically.

Key words: glued bent furniture panels, HDF, polyvinyl acetate (PVA) dispersion adhesive, polyurethane (PU) dispersion adhesive, bending strength, vacuum presses.

INTRODUCTION

The individual approach in furniture design nowadays leads to great competition of furniture manufacturers; more and more nonstandard solutions are sought in the vision and construction of the furniture. Composite materials have potential value for the furniture industry, both aesthetically and economically (Eckelman, 1993). The details are becoming more and more complex and require specialized technologies for making and lining details with a complex shape. Such structural details are: kitchen doors, door frames and wings, wall coverings and a number of other details to whose surfaces there are high requirements. Curved composite parts are a variant of the thin curvilinear details used in furniture constructions. With the mass penetration of wood fiber boards, as the main material for the production of frontal and glued shell structural elements for furniture, the most rational technologies and materials for their production and refinement are sought. There is data about studies on physical and mechanical characteristics of plywood (Shishkov, 1989; Kyuchukov, 1991; Garg AC, 1988; Navi and Sandberg, 2012) but there is no data about strength and deformation characteristics of structural elements made by plywood or HDF. The studies of how the type of adhesive effects on the physical and mechanical characteristics of the composite panels, such as HDF and plywood, are very few. According to Sandberg (2007), the properties of the adhesive, including curing time, adhesion, wettability of surfaces, antifriction, hardness and strength, are important parameters that can affect both the deformation of dimensional stability and the final hardness of the finished product. Temperature-humidity gradients appear in the process, which complicate the forming of an adhesive bond, with a constantly changing environment to create fixed adhesion properties. The adhesive bond between the adhesive and the veneer sheets was studied by Matuana et al. (1998) and using pulsed thermography by Berglind and Cassens (2003).

Several researchers point out that the properties of the final product depends on certain parameters of the material and the work process, e.g. variations in temperature and moisture content in the materials used (Hvattum et al. 1978), the design of the mold (Stevens and Turner, 1970; Lind 1981), the magnitude of the application pressure (Wu et al. 1999) and the quality and properties of individual materials used (Suchsland and McNatt, 1986; Ohya et al., 1989; Zemiar; Choma, 2002; Suchland, 2004).

MATERIALS AND METHODS

The test specimens are made of HDF boards (first series) with a thickness of 2.8 mm (produced by Kronospan, Bulgaria) and a density of 900 kg/m³. The plywood

(second series) used is manufactured by "WELDE Bulgaria" with a thickness of 4 mm and a density of 500 kg/m³. Two types of veneer were chosen as cladding materials - beech furniture veneer with a thickness of 0.6 mm and oak veneer with a thickness of 2.2 mm (supplied by J.A.F. Bulgaria). For statistical reliability of the results, 5 identical test specimens were prepared for each test with both types of veneer. A template with a radius of curvature of 100 mm was used for the production of the bent furniture panels. The test body consists of 5 lamellas with dimensions 260/100/2.8 mm glued by PVA dispersion – Jowacoll 103.05, PU dispersion - Jovapur 150.50 and polyurethane wood glue - SOUDAL 66A. The consumption norm of the adhesive used was determined by preliminary tests, so as to be the minimum at which the samples do not stick out -120 g/m^2 and the initial required adhesive strength of the facing materials is reached. The adhesive was applied unilaterally to the HDF slats, strictly following the consumption rate, by the weight method.



Figure 1: Laboratory vacuum press and the matrix for bending with a radius of curvature of 100 mm

For producing of the test samples was used laboratory vacuum press equipped with rubber membrane with a thickness of 3 mm. The force used for pressing the test samples is equivalent of the used vacuum of -0.08 MPa in the vacuum chamber. The gluing and the lining of the test samples is made

at once in a shortened overall technological regime, for studding the impact of the cladding material by the time of hardening of the adhesive on the whole surface of the bend furniture board. By preliminary experiments was determined the borderline radius of bending and gluing the lamellas made from

46 VLADIMIR MIHAILOV, TODOR PETKOV

HDF and plywood. The used matrix is a L-shaped detail with a radius of curvature of 150 mm. The test samples were loaded under

compression bending by collecting the shoulders. The testing was carried out by universal testing machine "Heckert – FP 100" – Germany (Figure 2).



Figure 2: The testing machine and the test installation.

A criterion was used to determine the strength of the test samples under compression loading is the maximum bending moment M_{max} (Simeonova, 2014), given by the formula:

$$M_{max} = F .1, [N.m]$$
 (1)

where:

F is the maximum strength under compression loading, [N];

l is the bending shoulder, [m].

The tests were carried out in temperature of the environment of $22 \pm 1^{\circ} C$ and humidity 63 ± 5 %. The statistically processed test data are presented in Table 1 with following indicators: average (X), standard deviation (S_x) , standard error (m_x) , variation coefficient (V_x) and coefficient of accuracy (P).

Type of glue	Aver. x	Sx	mx	Vx	Px
		bee	ech		
PVA	313.86	65.89	29.47	4341.73	0.065
PU disp. glue	428.81	25.87	11.57	669.20	0.065
PU glue	307.10	94.44	42.24	8919.37	0.065
		O	ak		
PVA	419.06	107.16	47.92	11482.82	0.065
PU disp. glue	497.26	32.06	14.34	1027.69	0.065
PU glue	401.76	99.57	44.53	9914.08	0.065

RESULTS AND ANALYSIS

From the carried-out experiments, it was found that for faultless production of bent-

glued details, it is essential to determine the time of reaching the given vacuum and the

duration of active vacuuming. In order to determine the time, required to achieve minimal adhesion strength, a preliminary study was carried out. The following values were determined for the three types of adhesives -30 min at a vacuum of -0.08 MPa, while by PU dispersion and polyurethane wood glue, it was necessary of using additional heat of 75°C. By the use of PU dispersion, that is necessary for activation of the adhesive and to obtain the adhesive forces between the glued lamellas. For polyurethane wood glue the additional heat is needed for shorting the time for hardening of the adhesive of 3 h (required time for cold bonding) to 30 min. After producing the test samples, they are left for fully hardening of the used adhesives for 7 days. After that time the test for determine

the bending strength by collecting the shoulders was carried out. On Fig. 3 are shown the average data of the bending strength of the bend furniture boards loaded in compression.

By the test samples glued with PVA dispersion, it can be seen bending strength of 313.86 N.m for the test samples lined with 0.6 mm beech veneer and 419.06 N.m for the test samples lined with 2 mm oak veneer. During the tests was observed that the samples were destroyed at the moment of destruction of the outer lamella and the veneer. The destruction is monitored by major cracks on the veneers and in the outer lamella loaded with critical bending stresses. Also, there can be seen places with delamination between the individual lamellas in the bent furniture board.

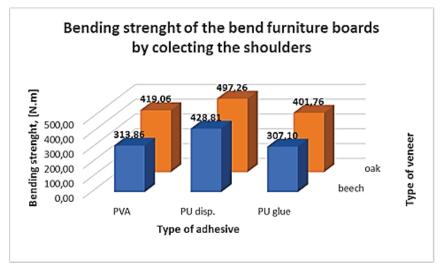


Figure 3: Bending strength of bend furniture boards.

By the test samples glued with PU dispersion, it can be seen bending strength of 428.81 N.m for the test samples lined with 0,6 mm beech veneer and 497.26 N.m for the test samples lined with 2 mm oak veneer. Using this type of adhesive shows the maximum bending moment values. During the tests was

observed that the samples were destroyed at the moment of destruction of the outer lamella and still standing until the veneer cracks (Figure. 4). The destruction is monitored by major cracks on the veneers and in the outer lamella loaded with critical bending stresses.





Figure 4: Test samples lined with 0.6 mm beech veneer.

By the test samples glued with PU wood glue, it can be seen bending strength of 307.10 N.m for the test samples lined with 0,6 mm beech veneer and 401.76 N.m for the test samples lined with 2 mm oak veneer. The collected data are similar to the usage of PVA adhesive, but the type of destruction is far different. During the tests was observed that

the samples were destroyed by the moment all of the lamellas have delamination one by one, until the last one lined with veneer is broken. The adhesive bonds are more flexible and the test samples are bouncing when the adhesive bond is destroyed. The full destruction of the test samples is when the veneer cracks with the last outer lamella (Figure 5).





Figure 5: Test samples lined with 2 mm oak veneer.

By the carried-out experiment the best values were observed by the test samples

made by using PU dispersion adhesive by bending strength of 428.81 N.m lined with

beech veneer and 497.26 N.m lined with oak veneer. The test samples lined with oak veneer gave higher bending strength, than those lined with beech veneer by all types of the used adhesives.

CONCLUSION

The results of the experimental studies give reason to do the following summarized conclusions:

- The highest bending stress under compression loading of the studied bend furniture boards have the test samples glued with PU dispersion adhesive and lined with 2 mm oak veneer, until the lowest result have the test samples glued with PU wood glue and lined with 0,6 mm beech veneer.
- Higher bending strength have the test samples lined with oak veneer glued with all of the examined types of used adhesives.

The type of glue affects on the end results of the bending strength of the bend furniture boards. For excellent result it is recommended to use PU dispersion adhesive with combination of the cladding material of oak veneer.

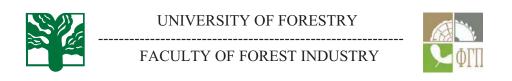
ACKNOWLEDGEMENTS

This paper was supported by the National Program "Young Scientists and Post-doctoral Students", Institution – University of Forestry, Faculty of Forest Industry

REFERENCES

- Berglind, H., Dillenz, A. 2003. Detection of glue deficiency in laminated wood with pulse thermography. Journal of Wood Science, 49(3), 216–220.
- ECKELMAN C. A. 1993. Forest products journal (USA) vol.49, № 2, ISSN: 0015-7473, p. 19–24.
- GARG, A. C. 1988. Delamination a damage mode in composite structures., Engineering Fracture Mechanics, Volume 29, p. 557–584.

- HVATTUM O., LIND P., OSVIK H. 1978. Springback of laminated bends. (Tech. Rep. No. 16). Blindern: Norsk Treteknisk Institut.
- KYUCHUKOV G., SHISHKOV I., DIMOVA L. 1991. Establishment of strength characteristics of plywood used in furniture construction. Study of mechanical properties of plywood panels, University study, Report, Sofia.
- LIND, P. 1981. Corner joints and laminated bends movements cause by moisture changes. (Tech. Rep. No. 26). Blindern: Norsk Treteknisk Institut.
- MATUANA, L. M., BALATINECZ, J. J. & PARK, C. B. 1998. Evaluation of adhesion between PVC and surface treated wood veneer laminates. Polymer Engineering and Science, 38(5), 765–773.
- MCNATT J. D. 1986. Computer simulation of laminated wood panel warp-ing, Forest Products Journal, 36(11–12), 16–23.
- NAVI P., SANDBERG D. 2012. Thermo-Hydro-Mechanical Processing of Wood. EPFL Press. Lausanne. Switzerland.
- OHYA S., KITAYAMA S., KAWAGUCHI M. 1989. The effect of veneer quality on the bending strength of laminated wood. Journal of the Japan Wood Research Society, 35(10), 905–911.
- SANDBERG D., NAVI P. 2007. Introduction to Thermohydro-mechanical (THM) Wood Processing, Handbook, ISSN: 1652-8433 ISBN: 978-91-7636-561-8.
- SHISHKOV I., KYUCHUKOV G., DIMOVA L., GEORGIEVA A. 1989. Establishment of strength characteristics of plywood used in furniture construction. Modulus of elasticity in bending University study, Report, Sofia.
- SIMEONOVA, R. 2014. Innovation of woodworking industry and engineering design, INNO, Sofia, 2/2014 (6): 93–101.
- STEVENS W. C., TURNER N. 1970. Solid and laminated wood bending. London: His Maj-esty's Stationery Office.
- SUCHSLAND, O. 2004. The swelling and shrinkage of wood. A practical technology primer. Madison: Forest Products Society.
- Wu Z. H., Furuno T., Zhang B. Y. 1999. Calculation models of pressure and position of curved laminated veneer lumber in molds during pressing. Journal of Wood Science, 45(3), 213–220.
- ZEMIAR, J., CHOMA, P. 2002. The shape stability of formed laminated wood. Wood Re-search (Drevarsky Vyskum), 47(2), 35–43.



INNOVATION IN WOODWORKING INDUSTRY AND ENGINEERING DESIGN

1/2021

INNO vol. IX Sofia

ISSN 1314-6149 e-ISSN 2367-6663

Indexed with and included in CABI

INNOVATION IN WOODWORKING INDUSTRY AND ENGINEERING DESIGN

Science Journal Vol. 10/p. 1–92 Sofia 1/2021

ISSN 1314-6149 e-ISSN 2367-6663

Edition of

FACULTY OF FOREST INDUSTRY - UNIVERSITY OF FORESTRY - SOFIA

The Scientific Journal is indexed with and included in CABI.

SCIENTIFIC EDITORIAL BOARD

Alfred Teischinger, PhD (Austria)
Alexander Petutschning, PhD (Austria)
Anna Danihelová, PhD (Slovakia)
Assia Marinova, PhD (Bulgaria)
Biborka Bartha, PhD (Romania)
Bojidar Dinkov, PhD (Bulgaria)
Danijela Domljan, PhD (Croatia)
Derya Ustaömer, PhD (Turkey)
Emilia-Adela Salcă, PhD (Romania)
George Mantanis, PhD (Greece)
Ivica Grbac, PhD (Croatia)
Ivo Valchev, PhD (Bulgaria)
Ján Sedliačik, PhD (Slovakia)
Jerzy Smardzewski, PhD (Poland)
Julia Mihajlova, PhD (Bulgaria)

Hubert Paluš, PhD (Slovakia)
Hülya Kalaycioğlu, PhD (Turkey)
Ladislav Dzurenda, PhD (Slovakia)
Marius Barbu, PhD (Romania)
Nencho Deliiski, DSc (Bulgaria)
Neno Tritchov, PhD (Bulgaria)
Panayot Panayotov, PhD (Bulgaria)
Pavlo Bekhta, PhD (Ukraine)
Silvana Prekrat, PhD (Croatia)
Štefan Barcík, PhD (Slovakia)
Valentin Shalaev, PhD (Russia)
Vasiliki Kamperidou (Greece)
Vesselin Brezin, PhD (Bulgaria)
Vladimir Koljozov, PhD (Macedonia)
Zhivko Gochev, PhD (Bulgaria)

EDITORIAL BOARD

N. Trichkov, PhD – Editor in Chief
D. Angelova, PhD – Co-editor
P. Vichev, PhD
N. Minkovski, PhD

Cover Design: DESISLAVA ANGELOVA

Printed by: INTEL ENTRANCE
Publisher address: UNIVERSITY OF FORESTRY — FACULTY OF FOREST INDUSTRY
Kliment Ohridski Bul., 10, Sofia, 1797, BULGARIA
http://inno.ltu.bg
http://www.scjournal-inno.com/

The Editorial Board wishes to thank the following reviewers for their contributions:

Ali Kasal, PhD (Turkey) Andrei Kavalov, PhD (Bulgaria) Anton Geffert, PhD (Czech Republic) Bilge Onaran, PhD (Turkey)

Borislav Kyuchukov, PhD (Bulgaria) Daniela Tesařová, PhD (Czech Republic)

Danylo Kosenko, PhD (Ukraine)
Diana Ivanova, PhD (Bulgaria)
Dorota Dziurka, PhD (Poland)
Ioannis Barboutis, PhD (Greece)
Elena Vladimirova, PhD (Russia)
Elena Pisareva, PhD (Bulgaria)
Emil Kichukov, PhD (Bulgaria)

Erika Loučanová, PhD (Slovak Republic)

Georgi Vukov, PhD (Bulgaria) Grzegorz Pinkowski, PhD (Poland) Hristo Shehtov, DSc (Bulgaria) Ioannis Ntintakis, PhD (Greece) Ivan Amudzhev, PhD (Bulgaria) Ivica Župčić, PhD (Croatia) Izabela Radkova, PhD (Bulgaria)

Jarmila Geffertová, PhD (Czech Republic)

Maria Evtimova, PhD (Czech Republi Maria Evtimova, PhD (Bulgaria) Marina Cionca, PhD (Romania) Michal Ferenčík, PhD (Czech Republic)

Mihai ISPAS, PhD (Romania) Milan Šimek, PhD (Czech Republic) Neli Staneva, PhD (Bulgaria) Nikolay Bardarov, PhD (Bulgaria)
Pavlin Vichev, PhD (Bulgaria)
Petar Antov, PhD (Bulgaria)
Pelin Yıldız, PhD (Turkey)
Petro Khomiuk, PhD (Ukraine)
Radostina Popova, PhD (Bulgaria)
Rangel Chipev, PhD (Bulgaria)
Regina Raycheva, PhD (Bulgaria)
Répet Németh, PhD (Hungary)
Rodica-Mariana Ion, PhD (Romania)
Roman Réh, PhD (Slovakia)

Sara Garcia, PhD (Portugal)
Sotir Glushkov, DSc (Bulgaria)
Stanimir Stoilov, PhD (Bulgaria)
Stela Tasheva, PhD (Bulgaria)
Stjepan Pervan, PhD (Croatia)
Tomasz Krystofiak, PhD (Poland)
Vasil Jivkov, PhD (Bulgaria)
Vasil Merdjanov, PhD (Bulgaria)
Vasil Vlasev, PhD (Bulgaria)
Victor Savov, PhD (Bulgaria)

Vladimir Karanakov, PhD (North Macedonia) Volodymyr Mayevskyy, PhD (Ukraine) Yancho Genchev, PhD (Bulgaria) Yusuf Erdil, PhD (Turkey) Zoran Janjić, PhD (Serbia)

Zoran Trposki, PhD (North Macedonia)

CONTENTS

CHECK OF SURFACE ROUGHNESS AVERAGE OF WENGE & MAPLE MILLING SURFACES	7
Ioannis Ntintakis, Andreas Onoufriou	
COMPATIBILITY OF HIGH SCHOOL DESK DIMENSIONS WITH ANTRHROPOMETRIC MEASUREMENTS1	4
Mehmet Acar, Yusuf Ziya Erdil, Ali Kasal	
INNOVATIVE FIREPROOF INSULATING PANELS FROM AGRICULTURAL WASTES 2	24
Yasmina Khalaf, Peter Hajj, Julia Mihajlova, Patrick Lacroix, Roland El Hage	
INFLUENCE OF HOT-PRESSING TEMPERATURE ON PROPERTIES OF ECO-FRIENDLY DRY-PROCESS FIBREBORDS WITH LIGNOSULFONATE ADHESIVE	29
Viktor Savov, Julia Mihajlova, Nikola Yotov, Bozhidar Madjarov	
POSSIBILITIES FOR UTILIZATION OF WASTE WATER AND RESIDUAL WOOD FIBRES IN THE PRODUCTION OF HARDBOARDS	37
Viktor Savov, Petar Antov, Nikolay Neykov	
INFLUENCE OF THE TYPE OF ADHESIVE ON THE PHYSICO-MECHANICAL PROPERTIES OF BEND FURNITURE BOARDS4	14
Vladimir Mihailov, Todor Petkov	
THE KINDERGARTEN INTERIOR AS AN IMPORTANT FACTOR FOR THE HEALTHY DEVELOPMENT OF PRESCHOOL CHILDREN5	50
Boris Iliev, Danijela Domljan	
THE DEVELOPMENT OF THE ENGINEERING DESIGN PROGRAM AT THE UNIVERSITY OF FORESTRY FROM THE VIEWPOINT OF ITS GRADUATES5	57
Pavlina Vodenova, Desislava Angelova	
OPPORTUNITIES FOR PRODUCT SERVICE SYSTEM DESIGN IN THE PROCESS OF FRANSITION TO A CIRCULAR ECONOMY6	58
Maya Ivanova	
PROJECT ASSIGNMENT AND PHASES OF IMPLEMENTATION IN INTERIOR DESIGN – THEORY AND PRACTICE7	74
Pavlina Vodenova	
AUGMENTED REALITY (AR) IN PUBLIC INTERIORS8	31
Stela Tasheva	
SCIENTIFIC JOURNAL "INNOVATIONS IN WOODWORKING INDUSTRY AND ENGINEERING DESIGN"	90