

## MATHEMATICAL DESCRIPTION OF THE CHANGE IN THE ATMOSPHERIC TEMPERATURE DURING DAYS AND NIGHTS

Nencho Deliiski, Neno Trichkov, Natalia Tumbarkova

University of Forestry, Sofia, Bulgaria

e-mail: deliiski@netbg.com, ntrichkov@gmail.com, ntumbarkova@abv.bg

### ABSTRACT

A mathematical description of the periodically changing during many days and nights temperature of the atmospheric air as a processing medium has been suggested. It is introduced in the boundary conditions of our own mutually connected 2D non-linear mathematical models of the logs' freezing and defrosting processes. For the numerical solving of the models a software program has been prepared in the calculation environment of Visual Fortran Professional. Results from a simulative investigation of the 2D non-stationary temperature distribution in beech logs with a diameter of 0.24 m, length of 0.48 m, moisture content of  $0.6 \text{ kg}\cdot\text{kg}^{-1}$ , and initial temperature of  $0 \text{ }^\circ\text{C}$  during their 5 days and nights continuous freezing and defrosting at sinusoidal change of the air temperature with initial values of  $-5 \text{ }^\circ\text{C}$  and different amplitudes are presented and analyzed.

**Key words:** mathematical description, atmospheric air, temperature, 2D models, beech logs, freezing, defrosting.

### INTRODUCTION

It is known that the duration and the energy consumption of the thermal treatment of frozen logs in the winter, aimed at their plasticizing for the production of veneer, depend on the degree of the logs' icing (Shubin 1990, Požgai et al. 1997, Trebula and Klement 2002, Videlov 2003, Pervan 2009, Deliiski 2009, 2013, Deliiski and Dzurenda 2010). In the accessible specialized literature there are reports about the temperature distribution in subjected to defrosting frozen logs only at conductive boundary conditions (Steinhagen 1986, 1991, Khattabi and Steinhagen 1993, 1995, Deliiski 2009, 2011, Hadjiski and Deliiski 2016).

The modelling and the multi-parameter study of the mutually connected freezing and defrosting processes of logs at atmospheric temperatures are of considerable scientific and practical interest. For example, as a result of such a study it is possible to determine the

real icing degree of logs depending on their dimensions, wood species, moisture content, and on the temperature of the air near the logs during their many days staying in an open warehouse before the thermal treatment in the production of veneer. The information about the real value of the icing degree can be used for scientifically based computing of the optimal, energy saving regimes for thermal treatment of each specific batch of logs.

The aim of the present work is to solve two own mutually connected 2-dimensional mathematical models of the transient non-linear heat conduction in logs during their freezing and defrosting at convective boundary conditions with periodically changing atmospheric temperature in the winter and to study the change in the resulting 2D non-stationary temperature distribution and icing degree of beech logs above the hygroscopic range.

### BOUNDARY CONDITIONS OF OWN 2D MATHEMATICAL MODELS OF LOGS' FREEZING AND DEFROSTING PROCESSES

In (Deliiski and Tumbarkova 2019) two mutually connected 2D non-linear mathematical models of the logs' freezing and subsequent defrosting processes are given.

$$\frac{\partial T(r,0,\tau)}{\partial r} = -\frac{\alpha_{wp-fr}(r,0,\tau)}{\lambda_{wp}(r,0,\tau)} \left[ T(r,0,\tau) - T_m(\tau) \right] \text{ at } T_m < 273.15 \text{ K}, \quad (1)$$

- along the longitudinal coordinate  $z$  on the logs' cylindrical surface during the freezing process:

$$\frac{\partial T(0,z,\tau)}{\partial z} = -\frac{\alpha_{wr-fr}(0,z,\tau)}{\lambda_{wr}(0,z,\tau)} \left[ T(0,z,\tau) - T_m(\tau) \right] \text{ at } T_m < 273.15 \text{ K}, \quad (2)$$

- along the radial coordinate  $r$  on the logs' frontal surface during the thawing process:

$$\frac{\partial T(r,0,\tau)}{\partial r} = -\frac{\alpha_{wp-dfr}(r,0,\tau)}{\lambda_{wp}(r,0,\tau)} \left[ T(r,0,\tau) - T_m(\tau) \right] \text{ at } T_m \geq 273.15 \text{ K}, \quad (3)$$

- along the longitudinal coordinate  $z$  on the logs' cylindrical surface during the thawing process:

$$\frac{\partial T(0,z,\tau)}{\partial z} = -\frac{\alpha_{wr-dfr}(0,z,\tau)}{\lambda_{wr}(0,z,\tau)} \left[ T(0,z,\tau) - T_m(\tau) \right] \text{ at } T_m \geq 273.15 \text{ K}, \quad (4)$$

where  $T$  is the temperature, K;  $\tau$  – time, s;  $\lambda_{wp}, \lambda_{wr}$  – thermal conductivity of the wood on the logs' surfaces in longitudinal and radial directions respectively,  $W \cdot m^{-1} \cdot K^{-1}$ ;  $\alpha_{wp-fr}, \alpha_{wr-fr}, \alpha_{wp-dfr},$  and  $\alpha_{wr-dfr}$  – convective heat transfer coefficients between the logs and surrounding air during the freezing and defrosting processes,  $W \cdot m^{-2} \cdot K^{-1}$ .

In (Deliiski and Tumbarkova 2019) mathematical descriptions of all variables in the models are given but the description of  $T_m$  only for the case of the freezing of logs in a freezer and of their subsequent defrosting at a room temperature is there presented.

These models have the following convective boundary conditions, in which the temperature of the processing air medium,  $T_m$ , as a variable participates:

- along the radial coordinate  $r$  on the logs' frontal surface during the freezing process:

### MATHEMATICAL DESCRIPTION OF THE CHANGE IN THE ATMOSPHERIC TEMPERATURE

For numerical solving of the mentioned above mutually connected mathematical models of the logs' freezing and defrosting processes it is needed to have a mathematical description of the temperature of the air medium of the surrounding environment in winter near the logs,  $T_m$ .

The periodic change of the atmospheric temperature  $T_m$  during the time at a constant value of its amplitude  $T_{ma}$  can be described

by the following equation (Gusenda and Ganowicz 1986, Deliiski 1988):

$$T_m = T_{m0} + (T_{ma} - T_{m0}) \cdot \sin(\omega \cdot \tau), \quad (5)$$

where  $T_{m0}$  is the initial value of  $T_m$ , K;  $T_{ma}$  – amplitude's value of  $T_m$ , K;  $\omega$  – angular frequency of change in  $T_m$ ,  $s^{-1}$ ;  $\tau$  – time, s. The angular frequency of  $T_m$  in eq. (5) is equal to

$$\omega = \frac{2\pi}{\tau_0}, \quad (6)$$

where  $\tau_0$  is the period of the change in  $T_m$ , s. For the precise solving of tasks with the participation of eqs. (5) and (6) it is needed to use  $\pi = 3.14159$ .

$$T_m = T_{m0} + [(T_{ma-in} - T_{m0}) \cdot (1 \pm K_{ma} \cdot \tau)] \cdot \sin(\omega \cdot \tau), \quad (7)$$

where  $K_{ma}$  is a coefficient equal to

$$K_{ma} = \frac{\Delta T_{ma-\tau_0}}{T_{ma-in} - T_{m0}}, \quad (8)$$

and  $\Delta T_{ma-\tau_0}$  is the change in  $T_{ma}$  during one period of  $\tau_0$ , K;  $T_{ma-in}$  – initial value of the amplitude, K.

The signs “+” and “–” in the right side of eq. (7) are used when the amplitude  $T_{ma}$  increases or decreases respectively during the periodically change in  $T_m$ .

If for example the initial value of  $T_{ma-in}$  is equal to 293.15 K,  $T_{m0} = 273.15$  K, and that value changes by  $\Delta T_{ma-\tau_0} = 2$  K during each period of  $\tau_0 = 1$  d = 86400 s, then according to eq. (8) it follows that

$$K_{ma} = \frac{2}{86400} = 1.15741 \cdot 10^{-6}.$$

## RESULTS AND DISCUSSION

The mathematical description of the periodically changing atmospheric temperature given above was introduced in the boundary

For a periodic change of the air temperature during one day and night, i.e. at  $\tau_0 = 1$  d = 24 h = 86400 s, according to eq. (6) it is obtained that

$$\omega = \frac{2\pi}{\tau_0} = \frac{2 \cdot 3.14159}{86400} = 7.2722 \cdot 10^{-5} s^{-1}.$$

When the amplitude of  $T_m$  gradually increases or decreases during the time compared to its initial value,  $T_{ma-in}$ , then the temperature  $T_m$  can be calculated according to the equation

conditions (1) to (4) of the mutually connected mathematical models of the logs' freezing and defrosting processes.

For the numerical solving of the models, a software program was prepared in the calculation environment of Visual FORTRAN Professional developed by Microsoft.

With the help of the program computations were made for the determination of the 2D non-stationary change of the temperature in the longitudinal sections of two beech logs named below as Log 1 and Log 2. The logs were with a diameter  $D = 240$  mm, length  $L = 480$  mm, basic density  $\rho_b = 560$   $kg \cdot m^{-3}$ , moisture content  $u = 0.6$   $kg \cdot kg^{-1}$ , and initial temperature  $t_{w0} = 0$  °C. Two options of 120 h continuous periodic freezing and defrosting of the logs have been studied as follows:

- for Log 1: at constant values of  $t_{m0} = -5$  °C and  $t_{ma} = 20$  °C;
- for Log 2: at constant value of  $t_{m0} = -5$  °C and at gradual decreasing of the amplitude's value  $t_{ma-in} = 20$  °C by 2 °C/d.

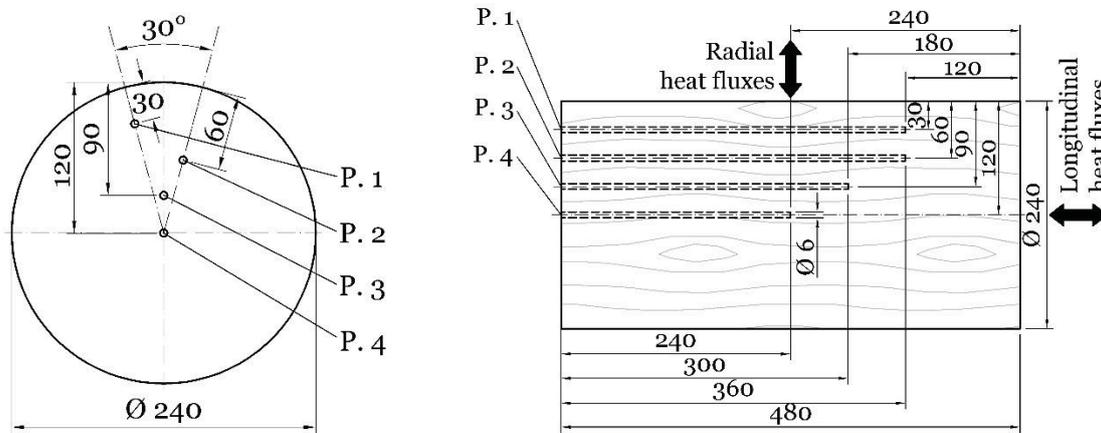
During the solving of the models, the mathematical description of the thermo-physical characteristics of beech wood with

fiber saturation point at 293.15 K (i.e. at 20 °C)  $u_{fsp}^{293.15} = 0.31 \text{ kg} \cdot \text{kg}^{-1}$  was used. At that value of  $u_{fsp}^{293.15}$  the studied logs contain a maximum possible bound water, equal to  $u_{fsp}^{272.15} = 0.331 \text{ kg} \cdot \text{kg}^{-1}$ . (Deliiski 2013). This means that at  $u = 0.6 \text{ kg} \cdot \text{kg}^{-1}$  the logs contain a free water, equal to  $0.6 - 0.331 = 0.269 \text{ kg} \cdot \text{kg}^{-1}$ .

The models have been solved with the help of explicit schemes of the finite difference method in a way, analogous to the one used and described in (Deliiski 2009, 2011, Deliiski and Tumbarkova 2019) for the solution of a model of the heating process of cylindrical wood materials. For this purpose, the calculation mesh has been built on  $\frac{1}{4}$  of the longitudinal section of the logs due to the circumstance that this  $\frac{1}{4}$  is mirror symmetrical towards the remaining  $\frac{3}{4}$  of the same section.

The models were solved with step  $\Delta r = \Delta z = 0.006 \text{ m}$  along the coordinates  $r$  and  $z$ . This means that the number of the steps along  $r$  was 20 and along  $z$  it was 40, i.e. the total number of the knots in the logs' longitudinal section was equal to  $N_{\text{total}} = 20 \times 40 = 800$ . The interval between the time levels,  $\Delta \tau$ , (i.e. the step along the time coordinate), has been determined by the software according to the condition of stability for explicit schemes of the finite difference method (Deliiski 2011) and in our case it was equal to 6 s.

On Figure 1 the coordinates of 4 characteristic points in the logs are given, in which the calculated change in the temperature  $t$  was registered and graphically presented. Point 1 is with  $r = 30 \text{ mm}$  and  $z = 120 \text{ mm}$ ; Point 2: with  $r = 60 \text{ mm}$  and  $z = 120 \text{ mm}$ ; Point 3: with  $r = 90 \text{ mm}$  and  $z = 180 \text{ mm}$  and Point 4: with  $r = 120 \text{ mm}$  and  $z = 240 \text{ mm}$  (center of the log).

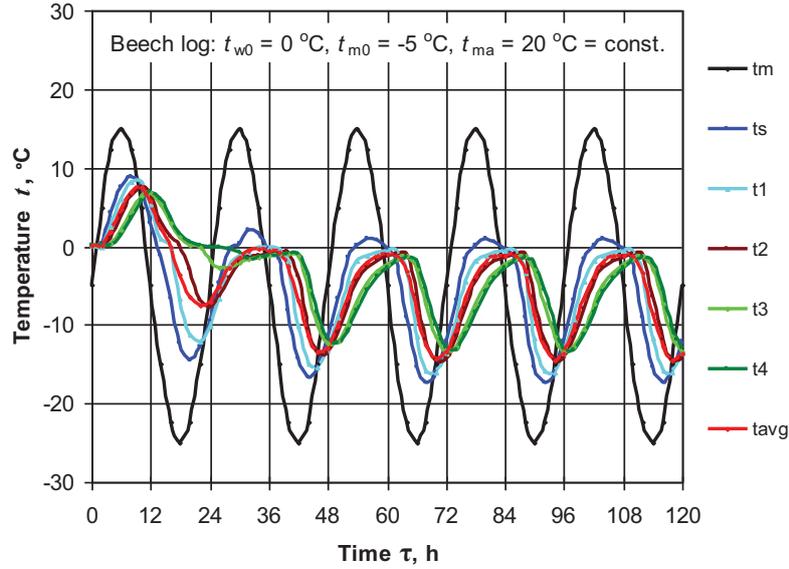


**Figure 1: Radial (left) and longitudinal (right) coordinates of 4 characteristic points for registration of the temperature change in logs subjected to periodically freezing and defrosting**

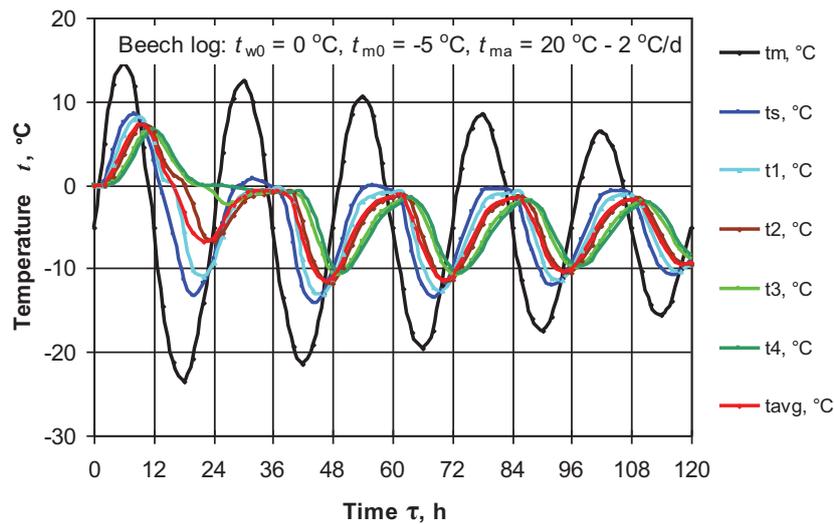
These coordinates of the characteristic points allow for the determination and analyzing of the 2D temperature distribution in logs during their freezing and defrosting.

Figure 2 and Figure 3 present the calculated change in temperature of the processing air medium,  $t_m$ , logs' surface temperature,  $t_s$ , logs' average mass temperature,  $t_{\text{avg}}$ , and  $t$  of

4 characteristic points in the studied beech logs during their periodic freezing and defrosting at constant values of  $t_{m0} = -5 \text{ °C}$  and  $t_{ma} = 20 \text{ °C}$  (Log 1) and at constant value of  $t_{m0} = -5 \text{ °C}$  and at gradual decreasing of the value of the amplitude  $t_{ma-in} = 20 \text{ °C}$  by  $2 \text{ °C/d}$  (Log 2) respectively.



**Figure 2:** Calculated with the model change in  $t_m$ ,  $t_s$ ,  $t_{avg}$ , and  $t$  of 4 characteristic points of the Log 1 during its 120 h periodically freezing and defrosting at constant values of  $t_{m0}$  and  $t_{ma}$



**Figure 3:** Calculated with the model change in  $t_m$ ,  $t_s$ ,  $t_{avg}$ , and  $t$  of 4 characteristic points of the Log 2 during its 120 h freezing and defrosting at constant value of  $t_{m0}$  and decreasing values of  $t_{ma}$  by 2 °C/d

On Figure 2 it can be seen that at constant values of  $t_{m0} = -5$  °C and  $t_{ma} = 20$  °C after 72<sup>nd</sup> h, i.e. after the 3<sup>rd</sup> period of  $t_m$ , a periodical change in the log's temperature with practically constant amplitudes for the separate points is coming. As far as the point is distanced from the logs' surfaces that much smaller is the amplitude of the periodic change of the temperature in that point. The amplitudes of  $t_m$  and  $t$  in the separate characteristic points after the 3<sup>rd</sup> period are equal to

as follows:  $t_{ma} = 20.0$  °C,  $t_{sa} = 9.5$  °C,  $t_{1a} = 8.2$  °C,  $t_{2a} = 7.2$  °C,  $t_{3a} = 6.5$  °C, and  $t_{4a} = 6.0$  °C.

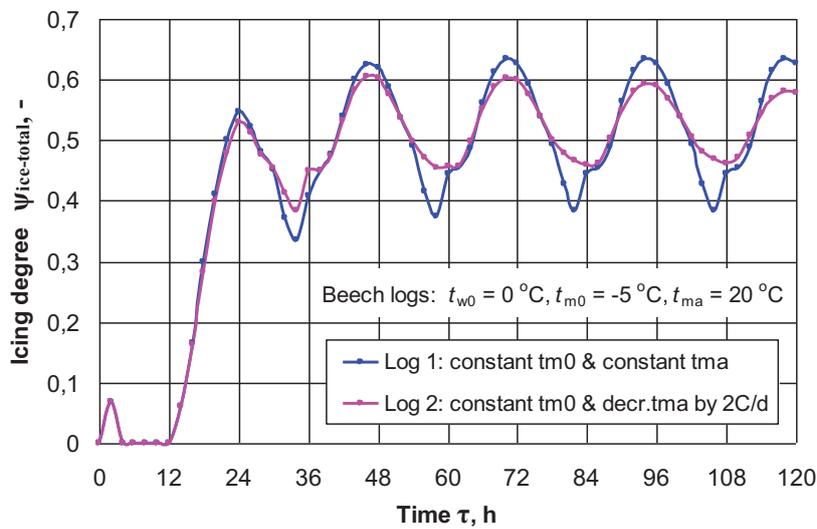
When  $t_{m0}$  remains constant and  $t_{ma}$  decreases during the time, the amplitudes of  $t$  in the separate characteristic points also gradually decrease (see Figure 3). At  $t_{m0} = -5$  °C = const and  $t_{ma} = 20$  °C - 2 °C/d, during the 5<sup>th</sup> period  $t_{ma} = 12.0$  °C,  $t_{sa} = 5.3$  °C,  $t_{1a} = 4.8$  °C,  $t_{2a} = 4.5$  °C,  $t_{3a} = 4.2$  °C, and  $t_{4a} = 4.0$  °C.

The average mass temperature of the logs,  $t_{avg}$ , at 120<sup>th</sup> h is equal to  $-13.56$  °C for Log 1 and to  $-9.23$  °C for Log 2.

Synchronously with the determination of the 2D non-stationary change of the temperature in the longitudinal sections of the studied logs, calculations of the change in their total icing degree,  $\Psi_{ice-total}$ , during the periodically freezing and defrosting have been carried out. These calculations were made according to the complex algorithm containing 9 steps, which are detailed in (Deliiski and Tumbarkova 2017).

Figure 4 presents the change in the icing degree  $\Psi_{ice-total}$  of the studied logs, which is caused by the freezing of both the free and bound water in them.

During the first 2 h of the 1<sup>st</sup> period of  $t_m$  the icing degree  $\Psi_{ice-total}$  increases from 0 to 0.07 due to the freezing of the free water only in some peripheral layers of the logs. From 2<sup>nd</sup> to 12<sup>th</sup> h of the 1<sup>st</sup> period  $\Psi_{ice-total}$  is equal to 0 because then the whole amount of the free and bound water in the logs is in a liquid state.



**Figure 4: Change in  $\Psi_{ice-total}$  during the periodically freezing and defrosting of the studied logs**

During the second half of the 1<sup>st</sup> period  $\Psi_{ice-total}$  increases from 0 to 0.55 for Log 1 and from 0 to 0.53 for Log 2. These values of  $\Psi_{ice-total}$  mean that 55% (i.e.  $0.33 \text{ kg}\cdot\text{kg}^{-1}$ ) from the whole amount of the moisture content of  $0.6 \text{ kg}\cdot\text{kg}^{-1}$  for Log 1 and 0.53% (i.e. approximately  $0.32 \text{ kg}\cdot\text{kg}^{-1}$ ) for Log 2 are then in frozen state.

After the 1<sup>st</sup> period the change in  $\Psi_{ice-total}$  is periodical and during the last 5<sup>th</sup> period of  $t_m$  it is in the range from 0.38 to 0.64 for Log 1 and for 0.46 to 0.58 for Log 2. At the end of the 5<sup>th</sup> period  $\Psi_{ice-total} = 0.627$  for Log 1 and  $\Psi_{ice-total} = 0.579$  for Log 2. These values of  $\Psi_{ice-total}$  mean that 62.7% (i.e.  $0.376 \text{ kg}\cdot\text{kg}^{-1}$ ) for Log 1 and 57.9% (i.e.  $0.347 \text{ kg}\cdot\text{kg}^{-1}$ ) for

Log 2 from the whole amount of the moisture content of  $0.6 \text{ kg}\cdot\text{kg}^{-1}$  are then in a frozen state.

The rest amounts of the moisture content  $u = 0.6 \text{ kg}\cdot\text{kg}^{-1}$ , i.e. 37.3% (i.e.  $0.224 \text{ kg}\cdot\text{kg}^{-1}$ ) for Log 1 and 42.1% (i.e.  $0.253 \text{ kg}\cdot\text{kg}^{-1}$ ) for Log 2 are in a liquid state in the cell walls of the logs at the end of 120 h periodic freezing and defrosting of the studied beech logs.

## CONCLUSIONS

This paper presents a methodology for mathematical modeling and research of two mutually connected problems: 2D non-stationary temperature distribution in logs subjected to many days and nights freezing and

defrosting at periodically changing air temperature near them in winter and change in the icing degree of the logs during these processes.

A mathematical description of the periodically changing atmospheric temperature in winter has been carried out. That description is introduced in our own mutually connected 2D non-linear mathematical models of the 2D temperature distribution in logs during their freezing and defrosting.

With the help of the model, computations for the determination of the temperature distribution and icing degree have been completed in calculation environment of Visual FORTRAN Professional for of two beech logs with a diameter of 0.24 m, length of 0.48 m, moisture content of  $0.6 \text{ kg} \cdot \text{kg}^{-1}$ , and initial temperature of  $0 \text{ }^\circ\text{C}$ , during their 5 days and nights continuous freezing and defrosting.

Two options of the periodic sinusoidal change in the air temperature near the logs have been studied: at constant initial value of  $-5 \text{ }^\circ\text{C}$  and constant amplitude of  $20 \text{ }^\circ\text{C}$  for Log 1 and at constant initial value of  $-5 \text{ }^\circ\text{C}$  and decreasing amplitude of  $20 \text{ }^\circ\text{C}$  by  $2 \text{ }^\circ\text{C}/\text{d}$  for Log 2.

It has been computed that after 120 h of the studied processes the total icing degree,  $\Psi_{\text{ice-total}}$ , of the logs reaches the following values:  $\Psi_{\text{ice-total}} = 0.627$  for Log 1 and  $\Psi_{\text{ice-total}} = 0.579$  for Log 2. This means that from the total amount of free and bound water in the logs, equal to  $0.6 \text{ kg} \cdot \text{kg}^{-1}$ , in a frozen state then are  $0.376 \text{ kg} \cdot \text{kg}^{-1}$  in Log 1 and  $0.347 \text{ kg} \cdot \text{kg}^{-1}$  in Log 2.

The solution of the models allows for the calculation of the temperature distribution and icing degrees, and also different energy characteristics of logs from diverse wood species for each desired moment during their freezing and defrosting at periodically changing atmospheric temperature with specific parameters. The results from the solutions

can be used for the development of scientifically based energy saving optimized regimes for thermal treatment of frozen logs with consideration of their specific icing degree and also in the software of systems for model predictive automatic control (Hadjiski and Deliiski 2016) of that treatment.

## REFERENCES

- DELIISKI, N. 1988. Thermische Frequenzkennlinien von wetterbeanspruchten Holzbalken. Holz als Roh- und Werkstoff, 46(2): 59–65, <https://doi.org/10.1007/BF02612530>.
- DELIISKI, N. 2009. Computation of the 2-dimensional transient temperature distribution and heat energy consumption of frozen and non-frozen logs. Wood Research 54(3): 67–78.
- DELIISKI, N. 2011. Transient heat conduction in capillary porous bodies. In: Convection and Conduction Heat Transfer. In Tech Publishing House, Rieka, 149–176 pp. <http://dx.doi.org/10.5772/21424>.
- DELIISKI, N. 2013. Modelling of the Energy Needed for Heating of Capillary Porous Bodies in Frozen and Non-frozen States. Lambert Academic Publishing, Scholars' Press, Saarbrücken, Germany, 116 p., <http://www.scholars-press.com/system/covergenerator/build/1060>.
- DELIISKI, N., DZURENDA, L. 2010. Modelling of the thermal processes in the technologies for wood thermal treatment. TU Zvolen, Slovakia, 224 p. (in Russian).
- DELIISKI, N., TUMBARKOVA, N. 2017. An Approach and an Algorithm for Computation of the Unsteady Icing Degrees of Logs Subjected to Freezing. Acta Facultatis Xilologiae Zvolen, 59(2): 91–104, [https://df.tuzvo.sk/sites/default/files/09-02-17\\_3\\_0\\_0\\_0\\_0.pdf](https://df.tuzvo.sk/sites/default/files/09-02-17_3_0_0_0_0.pdf).
- DELIISKI, N., TUMBARKOVA, N. 2019. Numerical Solution to Two-dimensional Freezing and Subsequent Defrosting of Logs. In Iranzo A editor. Heat and Mass Transfer – Advances in Science and Technology Applications, IntechOpen, 20 p., DOI: 10.5772/intechopen.84706, <http://mts.intechopen.com/articles/show/title/numerical-solution-to-two-dimensional-freezing-and-subsequent-defrosting-of-logs>.
- GUZENDA, E., GANOWICZ, R. 1986. Temperaturänderungen in brett-schichtverleimten Holzbalken bei periodisch wechselnden Umgebungstemperaturen. Holz als Roh- und Werkstoff, 44(2): 61–67.

- HADJISKI, M., DELIISKI, N. 2016. Advanced Control of the Wood Thermal Treatment Processing. Cybernetics and Information Technologies, Bulgarian Academy of Sciences, 16 (2): 179–197.
- KHATTABI, A., STEINHAGEN, H. P. 1993. Analysis of transient nonlinear heat conduction in wood using finite-difference solutions. Holz als Roh- und Werkstoff, 51, 272–278, <http://dx.doi.org/10.1007/BF02629373>.
- KHATTABI, A., STEINHAGEN, H. P. 1995. Update of “Numerical solution to two-dimensional heating of logs”. Holz als Roh- und Werkstoff, 53, 93–94, <http://dx.doi.org/10.1007/BF02716399>.
- PERVAN, S. 2009. Technology for Treatment of Wood with Water Steam. University in Zagreb (in Croatian).
- POŽGAJ, A., CHOVANEC, D., KURJATKO, S., BABIAK, M. 1997. Structure and Properties of Wood. 2nd edition, Priroda a.s., Bratislava, 485 p. (in Slovak).
- SHUBIN, G. S. 1990. Drying and Thermal Treatment of Wood. Lesnaya Promyshlennost, Moscow, URSS, 337 p. (in Russian).
- STEINHAGEN, H. P. 1986. Computerized Finite-difference Method to Calculate Transient Heat Conduction with Thawing. Wood Fiber Science, 18(3): 460–467.
- STEINHAGEN, H. P. 1991. Heat Transfer Computation for a Long, Frozen Log Heated in Agitated Water or Steam – A Practical Recipe. Holz als Roh- und Werkstoff, 49(7-8): 287–290, <http://dx.doi.org/10.1007/BF02663790>.
- TREBULA, P., KLEMENT., I. 2002. Drying and hydrothermal treatment of wood. Technical University in Zvolen, Slovakia, 449 p. (in Slovak).
- VIDELOV, H. 2003. Drying and thermal treatment of wood, University of Forestry, Sofia, 335 p. (in Bulgarian).



UNIVERSITY OF FORESTRY

---

FACULTY OF FOREST INDUSTRY



# **INNOVATION IN WOODWORKING INDUSTRY AND ENGINEERING DESIGN**

## **1/2020**

INNO vol. IX Sofia

ISSN 1314-6149  
e-ISSN 2367-6663

Indexed with and included in CABI

# INNOVATION IN WOODWORKING INDUSTRY AND ENGINEERING DESIGN

Science Journal

Vol. 09/p. 1–78

Sofia 1/2020

ISSN 1314-6149

e-ISSN 2367-6663

Edition of

**FACULTY OF FOREST INDUSTRY – UNIVERSITY OF FORESTRY – SOFIA**

**The Scientific Journal is indexed with and included in CABI.**

## SCIENTIFIC EDITORIAL BOARD

Alfred Teischinger, PhD (Austria)  
Alexander Petutschning, PhD (Austria)  
Anna Danihelová, PhD (Slovakia)  
Asia Marinova, PhD (Bulgaria)  
Bojidar Dinkov, PhD (Bulgaria)  
Danijela Domljan, PhD (Croatia)  
Derya Ustaömer, PhD (Turkey)  
George Mantanis, PhD (Greece)  
Ivica Grbac, PhD (Croatia)  
Ivo Valchev, PhD (Bulgaria)  
Ján Holécý, PhD (Slovakia)  
Ján Sedliačik, PhD (Slovakia)  
Julia Mihajlova, PhD (Bulgaria)  
Hubert Paluš, PhD (Slovakia)

Hülya Kalaycioğlu, PhD (Turkey)  
Ladislav Dzurenda, PhD (Slovakia)  
Marius Barbu, PhD (Romania)  
Nencho Deliiski, DSc (Bulgaria)  
Neno Tritchov, PhD (Bulgaria)  
Panayot Panayotov, PhD (Bulgaria)  
Pavlo Bekhta, PhD (Ukraine)  
Silvana Prekrat, PhD (Croatia)  
Štefan Barčík, PhD (Slovakia)  
Valentin Shalaev, PhD (Russia)  
Vasiliki Kamperidou (Greece)  
Vesselin Brezin, PhD (Bulgaria)  
Vladimir Koljozov, PhD (Macedonia)  
Zhivko Gochev, PhD (Bulgaria)

## EDITORIAL BOARD

N. Trichkov, PhD – Editor in Chief  
D. Angelova, PhD – Co-editor  
N. Minkovski, PhD

V. Savov, PhD  
P. Vichev, PhD

**Cover Design: DESISLAVA ANGELOVA**

**Printed by: INTEL ENTRANCE**

**Publisher address: UNIVERSITY OF FORESTRY – FACULTY OF FOREST INDUSTRY**

**Kliment Ohridski Bul., 10, Sofia, 1797, BULGARIA**

**<http://inno.ltu.bg>**

**<http://www.scjournal-inno.com/>**

**CONTENTS**

A METHODOLOGICAL APPROACH FOR NUMERICAL ANALYSIS OF UPHOLSTERED SOFA WITH FINITE ELEMENT METHOD (FEM) .....	7
Tolga Kuşkun, Ali Kasal, Ersan Güray, Recep Birgül, Yusuf Ziya Erdil	
INFLUENCE OF THE APPLIED PRESSURE ON FINGER JOINED END-TO-END WOOD.....	16
Todor Petkov, Vladimir Mihailov	
MATHEMATICAL DESCRIPTION OF THE CHANGE IN THE ATMOSPHERIC TEMPERATURE DURING DAYS AND NIGHTS .....	21
Nencho Deliiski, Neno Trichkov, Natalia Tumbarkova	
COMPUTATION OF THE AVERAGE MASS THERMAL CONDUCTIVITY OF OAK FURNITURE ELEMENTS SUBJECTED TO CONVECTIVE HEATING BEFORE LACQUERING .....	29
Nencho Deliiski, Neno Trichkov, Dimitar Angelski, Ladislav Dzurenda, Zhivko Gochev, Natalia Tumbarkova	
INFLUENCE OF UV RADIATION ON COLOR STABILITY OF NATURAL AND THERMALLY TREATED MAPLE WOOD WITH SATURATED WATER STEAM .....	36
Ladislav Dzurenda, Michal Dudiak, Adrián Banski	
PHYSICAL AND MECHANICAL PROPERTIES OF COMBINED WOOD-BASED PANELS WITH PARTICIPATION OF PARTICLES FROM VINE STICKS IN CORE LAYER .....	42
Rosen Grigorov, Julia Mihajlova, Viktor Savov	
ENGINEERING OF SELECTED PROPERTIES OF LIGHT MEDIUM DENSITY FIBREBOARDS PRODUCED FROM HARDWOOD TREE SPECIES .....	53
Viktor Savov	
EVALUATION OF VARIOUS LIGHTWEIGHT ARMCHAIRS IN TERMS OF ERGONOMICS .....	60
Mehmet Yuksel, Yusuf Ziya Erdil, Ali Kasal, Mehmet Acar	
AUTOMATION OF TECHNOLOGICAL OPERATIONS IN THE MANUFACTURE OF WOODEN TOYS.....	68
Izabela Radkova, Zornica Petrova	
SCIENTIFIC JOURNAL „INNOVATIONS IN WOODWORKING INDUSTRY AND ENGINEERING DESIGN“ .....	75